Modeling and Simulation of Nuclear Fuel Recycling Systems

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Outline

Introduction

Some applications to date

- Solvent extraction
- Plant-level modeling
- Agent design
- Key research needs
- Advancing to the future
 - NEAMS vision
 - Separations M&S development

Used Nuclear Fuel Recycling Entails Many Interconnected Steps



- Need new processes to meet future goals
- Emerging modeling and simulation capabilities can improve development and implementation (better, cheaper, faster)

Benefits of modeling and simulation of nuclear reprocessing systems

- Reduced cost of process development by guiding and minimizing the amount of experimental and piloting work required
 - Compare different separation and fuel cycle strategies
 - Develop new chemical processes with lower cost and waste generation
- Optimized system designs, with reduced design margins
 - Scale up with confidence
 - Reduce hot-cell footprint (surge capacity, throughput)
 - Process control
- Increased safety and acceptance of regulatory bodies
- Reduced risk of material diversion by providing accurate predictions of materials streams

Modeling and simulation

- Modeling is the development of an approximate mathematical description of physical and chemical processes at a given level of sophistication and understanding.
- Simulation utilizes computational methods to obtain predictions of process perform Important Note: Advanced
- "Together modeling and simulation do not replace the need for
 - enhance understanding of experiments!!!
 - provide qualitative/quantitative insights and guidance for experimental work, and
 - produce quantitative results that replace difficult, dangerous, or expensive experiments."

(Basic Research Needs for Advanced Nuclear Energy Systems, http://www.sc.doe.gov/bes/reports/abstracts.html#ANES)

Modeling and simulation of nuclear separations has primarily focused on solvent extraction



 $M^{+a_i}_{(aq)} + a_i NO^-_{3(aq)} + b_i TBP_{(org)} \Longleftrightarrow M(NO_3)_{a_i} \bullet b_i TBP_{(org)}$

$$K_{i} = \frac{\left[M(NO_{3})_{a_{i}} \bullet b_{i} TBP\right]_{org}}{\left[M^{+a_{i}}\right]_{aq} \left[NO_{3}^{-}\right]_{aq}^{a_{i}} \left[TBP\right]_{org}^{b_{i}}}$$





- Original predictions:
 - Graphical stage calculations using experimental equilibrium data and operating lines

Existing models are based on empirical fits to experimental data

$$K_{U} = \frac{\left[UO_{2}(NO_{3})_{2} \bullet 2 \ TBP\right]_{org}}{\left[UO_{2}^{2+}\right]_{aq} \left[NO_{3}^{-}\right]_{aq}^{2} \left[TBP\right]_{org}^{2}}$$

$$K_{Th} = \frac{\left[Th(NO_3)_4 \bullet 3 \ TBP\right]_{org}}{\left[Th^{4+}\right]_{aq} \left[NO_3^{-}\right]_{aq}^4 \left[TBP\right]_{org}^3}$$

$$K_{H}^{'} = \frac{\left[HNO_{3} \bullet 3 \ TBP\right]_{org}}{\left[H^{+}\right]_{aq} \left[NO_{3}^{-}\right]_{aq} \left[TBP\right]_{org}}$$

$$K_{U}^{'} = C_{1} + C_{2} \mu + C_{3} \mu^{2} + C_{2} \mu^{3}$$

$$K_{Th}^{'} = C_{5} + C_{6} \mu + C_{7} \mu^{2} + C_{8} \mu^{3}$$

$$K_{H}^{'} = C_{9} + C_{10} \mu + C_{11} \mu^{2} + C_{12} \mu^{3}$$

$$\mu \equiv \left[H^{+}\right] + 3\left[UO_{2}^{2+}\right] + 10\left[Th^{4+}\right]$$

Rainey and Watson, 1975



AMUSE Models Solvent Extraction



M. Regalbuto and C. Pereira, ANL

AMUSE has been used for process upset and product diversion analysis

- AMUSE was used to bracket the operational window for a plant conceptual design
 - Four fuel compositions were used as the initial process feed
 - High and low burn-up; long- and short-cooled fuels
 - Results showed little difference with cooling time but stronger effect due to burnup differences
- More recently AMUSE has been used to examine the effect of changing specific process parameters on the behavior of different elements
 - Design of instrumentation to track material
 - Process control
 - Product purity determination
 - Product diversion detection



Changes in feed composition lead to changes in the concentration profiles in the aqueous and organic phases

M. Regalbuto and C. Pereira, ANL

1980's – a full plant model

- Consolidated Fuel Reprocessing Program a complete plant simulation run in the Advanced System for Process ENgineering (ASPEN) simulator
- 52 components tracked throughout a preconceptual design of a plant containing 32 systems and approximately 700 streams, including:
 - fuel cleaning and storage
 - disassembly and shearing
 - dissolution and feed preparation
 - hulls drying
 - feed clarification
 - feed preparation and accountability
 - solvent extraction
 - solvent extraction ancillary systems (concentration, backcycle, storage, high-activity waste concentration, solvent recovery)
 - process support (acid and water recovery and recycle, process steam, and sump)
 - product conversion
 - cell atmosphere cooling and purification
 - process off-gas treatment
 - vitrification
 - vitrification off-gas treatment
- Large simulation for computers of the time
 - broken down into three segments that were executed separately to achieve a steadystate material balance for the complete plant.

Sandia Safeguards Performance Model



Advanced Monitoring System Results: Direct Diversions of 8 kg of Pu



B. B. Cipiti, SNL

Current state of separations process modeling

Solvent extraction most developed

- Useful aid in process development and analysis
- Semi-empirical fits
- Many species not modeled well, or not at all
- Leading codes use equilibrium stages
- Current codes do not predict well:
 - Mass transfer and reaction kinetics
 effects
 - Effects of micellization, third-phase formation, radiolysis, etc.
- Few transient codes
- Other important processes not well modeled
 - Legacy modules for some important unit operations are available
 - e.g., dissolver, acid recovery
- Full plant models are crude
 - Simple descriptions of important unit operations
 - Not fully transient



Height of bars indicates concentration of uranium in organic (top) and aqueous (bottom) phases in a 48-stage mixer settler bank. Time indicates the time in minutes from the start of operation with zero concentration throughout the system.

Sequestering agents are the basis for separations



Influence of ligand architecture

Large effects on binding affinity:



and significant impacts on selectivity:



Experimental development is slow and expensive



Computer-aided ligand development can acclerate progress



B.Hay, ORNL

Experimental validation

Extraction of Sr^{2+} from 1<u>M</u> HNO₃ using 0.1 M ligand in n-octanol, 25 °C



Extraction into t-butylbenzene from aqueous solution containing 1 M NaNO₃, 1.5 mM HNO₃, 0.1 mM Eu(N0₃)₃, and 1- μ L of ¹⁵⁵Eu tracer solution.



Lumetta, G. J.; Rapko, B. M.; Hay, B. P.; Gilbertson, R. D.; Weakly, T. J. R.; Hutchison, J. E. *J. Am. Chem. Soc.* **2002**, *124*, 5644.

B.Hay, ORNL

Recent workshops have identified key needs for contributions by modeling and simulation

Separations Challenges

- Plant-scale simulation
 - integrated toolset to enable full-scale simulation of a plant chemistry, mass transport, energy input, and physical layout
 - dynamic plant models
- Computational fluid dynamics
 - Multiple fluid phases, fully developed turbulence, non-Newtonian flows, interfacial phenomena, radical chemical processes due to the presence of ionizing radiation
- Predictive methods for thermodynamics and kinetics data as input to process simulators
 - extend currently limited thermodynamics data reliably into broader ranges of parameter spaces
 - incorporate limited experimental data and use computational chemistry approaches
- Rational design of the separations system from first-principles physics and chemistry
 - predict what molecules will have the desired properties and can be synthesized
 - reliably predict the properties of liquids, solvation, and kinetics in solution
- Connecting/crossing time and length scales, with uncertainty quantification
 - access longer times without dramatic changes in theoretical and algorithmic approaches
 - span spatial regimes; critical regime is the mesoscale (1 nm-1 μm)
 - Below 1 nm, computational chemistry; above 1 µm, continuum approaches

Data management and visualization

- Data must be captured, managed, integrated, and mined from a wide range of sources to enable the optimal design and operation of separation processes
- Computer resources and access
- Export control issues



http://www-fp.mcs.anl.gov/anes/SMANES /gnep06-final.pdf



http://www.sc.doe.gov/bes/reports/ abstracts.html#ANES

Advanced Modeling and Simulation has become an Essential Part of DOE-NE R&D



- **R&D Objective 1** Develop technologies and other solutions that can improve the reliability, sustain the safety, and extend the life of current reactors.
- R&D Objective 2 Develop improvements in the affordability of new reactors to enable nuclear energy to help meet the Administration's energy security and climate change goals.
- R&D Objective 3 Develop sustainable nuclear fuel cycles.
- R&D Objective 4 Understand and minimize the risks of nuclear proliferation and terrorism.

NEAMS Program Elements



- Integrated Performance and Safety Codes (IPSC)
 - Continuum level codes that will predict the performance and safety of nuclear energy systems technologies
 - Attributes include 3D, science based physics, high resolution, integrated systems
 - Using interoperability frameworks and modern software development techniques and tools
 - Program Support Elements
 - Develop crosscutting (i.e. more than one IPSC) required capabilities
 - Fundamental Methods and Models
 - Verification, Validation and Uncertainty Quantification
 - Capability Transfer
 - Enabling Computational Technologies

NEAMS Safeguards and Separations Scope



GOAL: Predictive capability for performance and safeguards aspects of reprocessing plants, to guide further research and development.

NEAMS Reprocessing Plant Simulator Toolkit

Vision

- Dynamic plant-level simulation capability encompassing entire plant and integrated safeguards
- Modules should be extensible, interoperable, and hierarchical to ensure continued usability
- Structured as a three-tiered collection of modules to aid in development and implementation
- Toolkit is open-source, but will enable use of controlled modules

Scientific Needs and Features

- Plant-level modeling and simulation of major sub-systems
- Dynamically coupled plant-level physicochemical modules.
- Integrated instrument models and inventory analysis modules.
- Loosely coupled unit operation modules as higher fidelity models
- Support stand-alone first-principles simulation capability
- Support analysis and design of alternative reprocessing technology
- · Support safeguards by design



Software Needs and Features

- Complex plant simulations through dynamic integration of user plug-in software modules
- Detailed visualization of realtime, dynamic simulation data and analysis
- Job launch capability on multiple computational platforms
- Distributed computing capabilities
- Support verification, validation, and uncertainty quantification
- Documentation and materials
 that facilitate usage of the toolkit

Plant-level models are under development for main unit operations. Example: Dissolver

Con	tactor	Speciation
	Continuous Process Countercurrent (intermittent solid flow) Rotary dissolver 	$\mathrm{UO}_{2(\mathrm{s})} + 2.7\mathrm{HNO}_{3} \longrightarrow \mathrm{UO}_{2}(\mathrm{NO}_{3})_{2} + 0.7\mathrm{NO}_{(\mathrm{g})} + 1.3\mathrm{H}_{2}\mathrm{O}_{(\mathrm{aq})}$
	 Prototype Rotary dissolver DOE Fuel Reprocessing Program 70-80's 0.5 ton/day HM full-scale ORNL 	$\mathrm{UO}_{2(\mathrm{s})} + 4\mathrm{HNO}_3 \xrightarrow{\mathrm{[HNO_3]} > 8\mathrm{M}} \mathrm{UO}_2(\mathrm{NO}_3)_2 + 2\mathrm{NO}_{2(\mathrm{g})} + 2\mathrm{H}_2\mathrm{O}_{(\mathrm{aq})}$
		$\mathrm{PuO}_{2(\mathrm{s})} + 4\mathrm{HNO}_3 \longrightarrow \mathrm{Pu(NO_3)_4} + 2\mathrm{H_2O_{(aq)}}$
	<i>k</i> th Stage "Liquid Volume Balance"	$\mathrm{FPO}_{1.18(\mathrm{s})} + 2.36\mathrm{HNO}_3 \longrightarrow \mathrm{FP(\mathrm{NO}_3)}_{2.36} + 1.18\mathrm{H_2O_{(\mathrm{aq})}}$
off-gas $k = 1$ example 1	$= -\underbrace{W(V_{\ell}^{(N)})}_{\text{perimentally measured (ORNL-TM-9019)}} + F^{n+1} k = 1, \dots N_s$	$\dot{m}_{\rm s} := K_{\rm s}^{(k)} \; [{\rm HNO_3}^{(k)}]^m f A_{\rm s} (\text{empirical rate law})$
product R	epresents a connection to the reprocessing toolkit nit-Ops Tier" which will compute this function from	$\left K_{\rm s}^{(k)} := \left(0.48 \exp\left(-0.091 \rho_{\rm s}^{\prime} \right) \right)^{w_{\rm UO_2}} \left(5 \exp\left(-0.27 \rho_{\rm s}^{\prime} \right) \right)^{(1-w_{\rm UO_2})} \right $
fir	st-principles continuum mechanics.	
Mass & Ene	rgy Balance	Thermodynamics
Mass & Ene Mass balance for each specie in the liquid phase of each stage:	$\begin{array}{c} \begin{array}{c} \text{rgy Balance} \\ \rho_{\text{UO}_2(\text{NO}_3)_2} & \rho_{\text{Pu}(\text{NO}_3)_4} \\ \rho_{\text{HNO}_3} & \rho_{\text{FP}(\text{NO}_3)_{2.36}} \end{array}$	Thermodynamics
Mass balance for each specie in the liquid phase of each stage: (k) = r(k)	$\begin{array}{c} \begin{array}{c} \text{rgy Balance} \\ \hline \rho_{\text{UO}_2(\text{NO}_3)_2} & \rho_{\text{Pu}(\text{NO}_3)_4} \\ \rho_{\text{HNO}_3} & \rho_{\text{FP}(\text{NO}_3)_{2.36}} \\ \rho_{\text{H}_2\text{O}} \\ \hline \end{array} \\ \hline \end{array}$	Thermodynamics Non-ideal liquid solution
Mass balance for each specie in the liquid phase of each stage: $d_t(\rho_i^{(k)}) \ V_\ell^{(k)} + \rho_i^{(k)} \ d_t(V_\ell^{(k)}) =$	st-principles continuum mechanics. rgy Balance $\rho_{UO_2(NO_3)_2}$ $\rho_{Pu(NO_3)_4}$ ρ_{HNO_3} $\rho_{FP(NO_3)_{2.36}}$ ρ_{H_2O} $= -F^{(k)} \rho_i^{(k)} + S_{\ell,i}^{(k)}$ ith species kth stage	Thermodynamics Non-ideal liquid solution (k) $D(U)$ (k) (k)
Mass balance for each specie in the liquid phase of each stage: $d_t(\rho_i^{(k)}) \ V_\ell^{(k)} + \rho_i^{(k)} \ d_t(V_\ell^{(k)}) =$ Mass balance for each specie in the solid phase of each stage:	st-principles continuum mechanics. rgy Balance $\rho_{UO_2(NO_3)_2}$ $\rho_{Pu(NO_3)_4}$ ρ_{HNO_3} $\rho_{FP(NO_3)_{2.36}}$ ρ_{H_2O} $= -F^{(k)} \rho_i^{(k)} + S_{\ell,i}^{(k)}$ ith species $n_{FPO_{1.18}}$ n_{PuO_2} n_{UO_2}	Thermodynamics Non-ideal liquid solution $ \rho_{\ell}^{(k)} = R(T, P, \rho_{\mathrm{H_2O}}^{(k)}, \rho_{\mathrm{HNO_3}}^{(k)}, \rho_{\mathrm{UO_2(NO_3)_2}}^{(k)}) $
Mass balance for each specie in the liquid phase of each stage: $d_t(\rho_i^{(k)}) \ V_\ell^{(k)} + \rho_i^{(k)} \ d_t(V_\ell^{(k)}) =$ Mass balance for each specie in the solid phase of each stage: $\rho_s \ d_t(V_s^{(k)}) = -\dot{m}_s^{(k)}(V_s^{(k)}) +$	$\begin{array}{c} \begin{array}{c} \text{rgy Balance} \\ \hline \rho_{\text{UO}_2(\text{NO}_3)_2} & \rho_{\text{Pu}(\text{NO}_3)_4} \\ \rho_{\text{HNO}_3} & \rho_{\text{FP}(\text{NO}_3)_{2.36}} \\ \rho_{\text{H}_2\text{O}} \\ \hline \end{array} \\ \hline = -F^{(k)} & \rho_i^{(k)} + S_{\ell,i}^{(k)} \\ \hline \end{array} \\ \begin{array}{c} \text{ith species} \\ k\text{th stage} \\ \\ n_{\text{FPO}_{1.18}} & n_{\text{PuO}_2} & n_{\text{UO}_2} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} \text{ith species} \\ k\text{th stage} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array}$	Thermodynamics Non-ideal liquid solution $\rho_{\ell}^{(k)} = R(T, P, \rho_{\mathrm{H_2O}}^{(k)}, \rho_{\mathrm{HNO_3}}^{(k)}, \rho_{\mathrm{UO_2(NO_3)_2}}^{(k)})$

Modern M&S for Solvent Extraction



Centrifugal Contactor Simulations Using Open-Source CFD

Goal – Provide a pathway for:

- Predicting stage efficiency for given conditions
- Developing lower fidelity models for plant-level unit operations models FY10 Results
- Finite Element-based (unstructured) Lattice Boltzmann Method (FELBM)
 - Testing of modifications to code's solver and BC implementation
 - Verified excellent parallel scaling performance up to 2048 cores on Argonne's BlueGene/P
- OpenFOAM
 - Demonstration of limits to approach for three phase liquid-liquid-air simulation
 - Coupled mixing/separation zone contactor models exploring BC and mesh dependence







Animation of Liquid-Liquid Mixing



Comparison of effect of vane geometry on mixing













Interface with Experimental Work Contactor CFD Validation Using Electrical Resistance Tomography (ERT)



Circular 32-Electrode Array Tomography Data: 4-Vane



Wang, M. Meas. Sci. Technol. 13:101 (2002).



- Acquired data is a temporal and spatial average
 - Temporal: ~0.75 s (overall rate of ~1.4 Hz)
 - Spatial:
 - Out of plane: electrode size, 7.6mm x 7.6mm
 - In plane: ITS quotes 5% of vessel diameter (5% of 6" = 0.3" = 7.6mm)
- Approximate vane location is shown
 - Measurements are relative to a reference measurement (avg of 100 frames)
 - Effect of internals is masked
- Tomographic "reconstruction" based on Sensitivity Conjugate Gradient (SCG) method [Wang 2002]
- Result is generally asymmetric
 - This was unexpected, but feed is also asymmetric
 - Addition of windows to vane plate could visually verify this result

Flow Regime Visualization

- State-of-the-art high-speed digital video imaging, solid-state light, and optics provide needed insight
- > Sub-millimeter flow regime never seen before
- Reveals significant time and length scales under realistic system and operating conditions





• Elapsed time: 37 ms

Spatial resolution: ~7 µm

Organic-rich flow regimes possess greater air entrainment

• Elapsed time: 18.5 ms



seeing is believing . . .

These videos provide more than insight for modeling . . .

V. de Almeida, ORNL

Computer-Aided Image Analysis

- Large data sets are obtained (8 GB for 1-s elapsed time)
- Can utilize powerful tools of computer image analysis (machine vision)
- Computing intensive need to inspect every pixel and its vicinity



Solvent Extraction Agent Design

HostDesigner code parallelized for minor actinides solvent extraction agent design

- > Previous simulation capability: limited MM analysis on 10 to 20 ligands (~days wall-clock time)
- Current capability: MM conformer search on > 1000 ligands in ~1.5 hours wall-clock time



Current focus:

- Improving functionality by adding quantum mechanics based scoring of candidates
- Improving computing throughput by embedding a quantum mechanics library in HostDesigner



Chemical Transport

Important chemical reactions occur at the interface

Challenges

- Lack of basic understanding of how species move across interfacial "region"
- Strongly coupled physical and chemical processes

An approach to understand solvent extraction

- Molecular dynamics simulation
- Calibration from experimental data
- Insight from molecular quantum chemistry calculations when experimental data are not available

?



Interfacial Transport "Visualization" by Molecular Dynamics Simulation



All uranyl adsorbed on interface
 Some nitrate ion also adsorbed



Onset of extraction of UO₂²⁺, NO₃⁻, H₂O
 Species have crossed the TBP surfactant layer

ightarrow H₂O and organic hidden; TBP butyl tails hidden





Phys. Chem. Chem. Phys., 2010, **12**, 15406–15409 Solv. Extr. Ion Exch., 2010, **28**, 1–18 J. Phys. Chem. B 2009, **113**, 9852–9862

V. de Almeida, ORNL

DB: five_cmp-0001.pdb



Ditturon;1-12-00001,pdb



Quantifying Water Extraction by TBP/Dodecane via MD



> Molecular dynamics of aqueous/organic interfacial transport of water

- Modeling TBP (QM parameterized)
- Testing various FF: AMBER, CHARMM, GROMOS, OPLS
- Large scale simulation 1 M atoms (ORNL/INL machines)
- Prediction of thermodynamic (density/enthalpy) and transport properties
- Extraction simulations in progress

Sharp Interface Tracking in Rotating Microflows of Solvent Extraction



Water-TBP-NDD

- Front tracking two-phase flow

3 mm

- Development of incompressible flow, high-order accuracy interface tracking
- Simulation on New York Blue Gene (1024 cores)
- Porting code to INL machines
- Further development on correcting interface impermeability

E-chem modeling

- **Goal: Predictive capability of electrorefiner** performance
- Phenomena in an electro-refiner include:

Solid electro-dissolution, Electrohydrodynamics, Electrodeposition composition and electrode morphology, Thermodynamics, Electro-chemical reaction

Recent Progress: Initial model developed. Results for codeposition of metals at cathodes are in agreement with experimental studies

- •Uses current available data for activity and diffusion coefficients, apparent standard electro-potential; assumes the fuel is an ideal solid solution
- Considers surface area changes due to dissolution and deposition
- Calculates behaviors of co-dissolution at the solid anode and co-deposition at the solid cathode of Zr-U-Pu alloys.





FY15 Target:

Model that incorporates electrochemical kinetics, phase morphology, and property data.

Cd

Example of Safeguards Modeling: Neutron Balance Approach for Head-end Safeguards

- Concept: Correlate number of neutrons escaping fuel bundle to number escaping Input Accountability Tank (IAT).
- Used nuclear fuel emits spontaneous and (α,n) neutrons primarily from ²⁴⁴Cm.
- The ratio of Cm/Pu can be determined from burnup to yield Pu mass in both places.
- The number of neutrons emitted/gram from the used fuel in an assembly should be the same as in an Input Accountability Tank (IAT); only these two locations in the plant are currently analyzed.

Methodology:

- Isotopic composition estimates of fuel assemblies calculated using Monte Carlo burnup
- Determine neutron source terms and use MCNP for transport and multiplication calculations



Example of Instrumentation Modeling: Hybrid K-Edge Modeling

- Hybrid K-Edge method uses two simultaneous xray measurement techniques to determine the actinide content of a liquid sample
- GOAL of the Modeling Activity: Simulate the act of measuring a liquid specimen with a hybrid densitometer
 - Develop a safeguards module for Hybrid K-Edge/X-ray Fluorescence Densitometer (HKED) simulation
 - The module will read user-defined input parameters (including simulated concentrations of thorium, uranium, neptunium, plutonium, americium, and curium) into the plant-level code and produce the desired spectra.



Photorealistic and Physics-Realistic Interactive Models for Test, Evaluation and Analysis



- Model built and textured from scratch in 1.5 work days by the Los Alamos National Laboratory VISIBLE development team, using only photos of the original equipment.
- Each part of the modeled equipment can be manipulated and custom programmed for behavior.

K. Michel, LANL

Real-world vs. Virtual World





A virtual model can have as much, or as little detail as needed.









K. Michel, LANL

Future Safeguards Data Review Interface: Safeguards Data Shown in Context for Evaluation and Analysis of Events



105

SW1 Fission Chamber A

 10^{3}

105

SE1 Fission Chamber A

103

08/31/92 00:00:00



Summary

- Modeling and simulation have provided useful input to the development of fuel cycle separations over the past several decades.
- With significant scientific advancements and vast increases in computational power, modeling and simulation can play an increasing role in solving the complex challenges to be overcome in developing advanced nuclear energy systems.

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